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Review

Surface Modification of Carbon Fibers

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Abstract: The purpose of the review is to provide new insight into the potential of surface modification of carbon fibers for enhancing the application of the carbon fibers many a fold. To this end a total of 429 papers on the subject of surface modification of carbon fibers by a variety of chemical and electrochemical methods published during the period from 2010-2022 have been reviewed. Astounding results of surface functionalization of carbon fibers by a variety of state of the art methods resulting in the unconventional applications of the resulting modified carbon fibers are summarized in a nut-shell in schemes from 1-6 towards the end of the review. Surface modification induces functionality to carbon fibers (CFs). The vitality of CF surface modification reactions could only be compared to the life process of respiration that sustains the multi functionality of living cells. Applicability of CFs can be drastically enhanced in incomprehensible ways by surface modification. Upon surface modification, inert and non-reactive CF surface becomes chemically active and functional with utility in diverse fields, namely, health, energy, environment, defense, catalysis, smart materials and many others. Surface modification methods can be broadly classified into chemical, electrochemical and physical methods. By these surface modification methods, the inert FC surface becomes polar. Surface properties like roughness, wettability and energy are enhanced. Modification processes like sizing, oxidation, amination, silanization, polymerization, nanoarchitecture induces multifunctionality on CF surface. Modified CFs when used as reinforcing material in carbon fiber reinforced plastics (CFRPs), improved bonding at the interface with resin matrices is observed with enhanced and outstanding mechanical properties (flexural strength, flexural modulus, IFSS, ILSS, hardness, elastic modulus, bending strength and compression strength).

Keywords: carbon fibers; surface modification; chemical; sizing; nanomaterials; oxidation; electrochemical; grafting; physical; modification; functionalization; multifunctionality; CFRPs; interface;, mechanical property

1. Introduction

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Carbon fiber (CF) reinforced epoxy composites are widely used in aerospace engineering structures like, aerospace vehicles, rockets and artificial satellites owing to their excellent specific mechanical properties [1]. Carbon fibers are appropriate reinforcing material for the polymer matrix. Carbon fibers have high specific tensile strength, high modulus, and outstanding wear resistance, and are widely used for the reinforcement of advanced composite materials. CF reinforced thermoplastic composites are of interest owing to their easy processability and recycling [2]. However, the problem is that the carbon fiber surface is chemically non-polar and inert. As a result, as such carbon fibers cannot adhere strongly to the polymer matrix. It is the region between the carbon fiber (reinforcing material) and the filler matrix (polymer resin), termed as interface, which is crucial, vital and key for the ultimate performance of the CFRPs and their advanced applictions. As a result of poor adhesion between CF and polymer matrix, the strength of interfacial bonds is week and hinders the achievement of ideal mechanical properties of the composites. The structure and properties of the interface play a key role in the high temperature resistance and mechanical behavior of the integrated structure of composites. Better interface between the CF and the matrix effectively ensures the transfer of the stress load from the matrix to the CF increasing the application of CFRP's many a fold [1]. Carbon fiber reinforced polymers (CFRP's) are emerging as metal substitutes with

applications in space exploration, military aircraft components, ship and submarine manufacturing, renewable energy industry (as blades of wind turbine), and automobile industry. In principle, CFRP's can be used in all the applications where light weight and high strength of the materials is required.

The problem of adhesion between the carbon fiber and polymer matrix can be solved by inducing polarity on to carbon fiber surface. There is a saying in Chemistry that "Like dissolves like". Since the polymer matrix is polar, by modifying the surface of CFs to be polar, makes them adhere strongly with the polymer matrix via strong covalent bonding interactions. Surface modification of CF is a well-known method to generate surface functional groups and thereby increase the interfacial adhesion between CF and the surrounding polymer matrix. The process of sizing the carbon fibers is one of the fundamental and key processes in the manufacturing of carbon fibers to induce surface polarity [3]. Oxygen rich surface functional groups can be generated on CF surface via different methods, namely, (a) oxidative treatment of CF's with a mixture of conc. H₂SO₄/conc. HNO₃, oxidation with conc. HNO₃, treatment with aq. (NH₄)₂CO₃, oxyfluorination, anodic oxidation and ozone treatment [2] and by a variety of physicochemical activation methods [4]. With the increase in polar functional groups and the wettability of CF, their surface roughness is increased; mechanical properties like the interfacial shear strength (IFSS), inter-laminar shear strength (ILSS) and impact toughness are enhanced. IFSS is a critical measure indicative of the interfacial adhesion between CF and polymer matrix [5]. Once the surface of the CFs is sufficiently charged, the CFs can reinforce strongly with the polymer matrix with well-defined composition, structure and properties at the interface. The bonding at the interface determines the ultimate performance of composites. Sizing is a commercial process for improving the compatibility of CF with polymer matrix with strong interfacial bonding. Owing to the significance as well as challenge of producing CFRPs with strong interface, novel and innovate methods, like modification of carbon fibers with sizing, the subject of the present review, need to be developed for improving the adhesion of CF's with the polymer matrix.

2. Role and Characterization of Sizing Agent Used for the Modification of Carbon Fibers:

2.1. Role of Sizing Agent in Enhancing the Interfacial Strength of CFRP's:

Sizing process is defined as a potential chemical method of modifying the surface of the carbon fibers. As a result of sizing the surface of carbon fibers becomes polar enriched with heteroatom (oxygen/nitrogen/sulphur) containing function groups. As a result of sizing process, CF becomes chemically more reactive with the resin matrix facilitating stronger interface formation in the CFRPs. Sizing process has commercial significance and so, much of the knowledge of sizing process, sizing agents used, sizing composition are often a subject of intellectual property [6–8] and only limited details are available in open literature [9–12]. Among several types of sizing agents, namely, epoxy resin, unsaturated resin and thermoplastic resin, the epoxy resins (for example, E44 , E51) are most widely used. Chemical structures of epoxy sizing agents E51, dimer of DGEBA (diglycedyl ether of bisphenol A), and E44, hydroxy propyl derivative of DGEBA, are shown in Figure 1 [3,13]. The carbon and proton nuclei in different chemical environments are numbered and alphabeted respectively. The choice and selection of the sizing agent for modifying the CF surface is largely based on the application dictated by the polymer resin matrix used in the preparation of carbon fiber reinforced plastics (CFRPs) [3].

Figure 1. Chemical Structure of epoxy resin based sizing agent, E44, hydroxyl propyl derivative of **diglycedyl ether of bisphenol A (**DGEBA) [3]. Adapted from reference 3 with permission from Elsevier.

The structure of strongly polar unsaturated resin, N-(4′4-diaminodiphenyl methane)-2 hydroxypropyl methacrylate (DMHM), that was used as sizing agent for CF (polyacryl nitrile based) is shown in Figure 2. A two fold enhancement in IFSS is observed upon using DMHM as sizing agent instead of the epoxy type sizing agent, E44 [3].

Figure 2. Unsaturated resin, N-(4′4-diaminodiphenyl methane)-2 hydroxypropyl methacrylate (DMHM), with strong polarity. Adapted from reference 3 with permission from Elsevier.

Thermoplastic resins are another class of sizing agents. Thermoplastics are different from thermosetting plastics. Typical examples of thermoplastics include, polyethylene (PE), polypropylene (PP), acrylonitrile butadiene styrene (ABS), polyamide (PA), polycarbonate (PC), polyether ether ketone (PEEK), polyetherimide (PEI), and polyether sulfone (PES). Typical advantages of thermoplastics being a choice of sizing compound/resin matrix is that they do not require curing stage, less hazardous chemical composition, improved recycling convenience and large scale production capability [2,14].

CF play crucial role as load bearing component in CFRPs. Owing to the merits of CF, CFRPs are used as a replacement to metal components in high tech fields like aerospace, automotive, wind energy, marine turbine blades. A comparison of the thermo-physical properties of CF with graphite fiber and Al metal shows the superiority of CFs with lower density value (ϱ , g/cm³), modest heat capacity $(J/g/K)$ and thermal conductivity (W/mK) values (where g, cm, J, m and K refers to gram, centimeter, Joule, meter and Kelvi) as shown in Table 1 [15].

	. .		
Material	σ (g/cm ³)	C_{p} (J/g/K)	(W/mK)
Carbon fiber, CF	1.6	0.676	900
Graphite fiber, GF	っっ	0.71	$100^{\rm a}$ (38 ^b)
Aluminum	7 ל	0.895	237

Table 1. Thermo-physical properties of graphite fiber, carbon fiber and Al [15].

Note: a - parallel to graphite layers; b - perpendicular to graphite layers;

Use of CFRPs is particularly advantageous over metals in space vehicles (like rocket motors, and satellites) as the amount of fuel needed to put a small weight into space is reduced considerably. Other metal replacements include helicopter blades, air craft structural components, air craft containers and chemical and ship building industries. In fact, the first ever carbon fibers were made by a group at Royal air craft establishment (RAE) with good tensile properties for high performance reinforcement applications [16]. As early as 1971, Jeffries has correctly assessed the potential of CFs and their unique properties making them ideal candidates for diverse application. Any engineering device involving rotating component will obviously be improved in its performance if manufactured from CFRP. This is because the centrifugal forces in the rotating part are dependent on the weight of the part. The structure of carbon fibers is similar to graphite. The carbon atoms are in layers or planes which are arranged almost parallel to each other. In true graphite, the atoms in each plane are arranged in a regular manner with respect to those in the adjacent planes. On the contrary, in CF, there is no such regular arrangement and the structure is described as turbostratic [16].

Typical demerits of CFs namely, the smooth, non-polar, chemically inert surface with poor wettability and adhesion to resin (polymer) matrix, can be surmounted by the process of sizing [17]. Sizing process reduces the surface defects caused during fiber production process and thereby leads to improved adhesion with the resin matrix and results in enhanced mechanical properties [18]. Sizing agent performs multiple roles, namely, protecting the CF during processing, providing active functional groups on the surface of CF and improving the wettability of CF surface and the compatibility between CF and resin matrix. Solution and emulsion are the two types of sizing agents usually employed. Solution type sizing agent requires large amount of organic solvent while emulsion type comprise of organic resin dispersed in water with the help of an emulsifier. Emulsion type sizing agents are environmentally friendly and are safe to handle and so predominantly used compared to the solution type sizing agents [12]. The pH value of the sizing agent affects the IFSS of the CFRP as shown in Figure 3. Emulsion type sizing agent with dispersed reduced graphene oxide (rGO) was used to size the CF's with a concentration of 2 %. The sizing agent with acidic or neutral pH value has a minor influence on the improvement of IFSS of CF-epoxy composite. Optimum value of IFSS (92.3 MPa) was observed when the pH value of the sizing agent is 10.5. Beyond a pH value of 10.5, the IFSS value varied only slightly. When the pH value of the sizing agent increased to 12, the sizing agent became unstable due to deemulsification. ~ 20.3 % improvement in IFSS of the CF-epoxy (E51) composite is achieved when the pH of the sizing agent is increased from 4.2 to 10.5 [12]. Increasing the mechanical properties of CFRPs is a challenge and a requirement from the high technology sector like missile applications [19].

Figure 3. Effect of pH of sizing agent on the interfacial shear strength (IFSS) of CFRP. Adapted from reference 12 with permission from John Wiley and Sons.

Typical example of the measurement of the vital property of the CFRP, namely, IFSS is depicted in Figure 4. The IFSS between the single carbon fiber (SYT49) (sized with rGO modified epoxy based emulsion type sizing agent) and the resin microdroplets (E51) is determined by micro de-bonding test carried out on a interfacial evaluation equipment. The carbon fiber single filament is taped on the iron frame work. Resin microdroplets (E51) are wetted on the surface of the fiber. The resin microdroplets formed on the single fiber taped to the sample holder were cured by placing the sample in air oven at the curing conditions of 80 °C for 3 h, 140 °C for 1 h and 150 °C for 1 h. The temperature programming of the curing process is dependent on the resin matrix used in the CF-epoxy composite preparation. Two metal blades were clamped near a particular resin droplet and the sample holder is moved (in the direction of V) at a speed of 5 mm/min during the IFSS measurement. The metal

blades were fixed during the test. The embedded length of the measured microdroplet of the resin $(ln; \mu m)$ is approximately 40-60 μm . The parameter measured during this test is the maximum force (Fmax) required to de-bond a particular resin microdroplet from the single carbon fiber. The IFSS value of the composite is deduced by substituting the value of F_{max} in the following equation (1) [12,20]:

$$
IFSS\ (MPa) = \frac{F_{max}}{\pi d_f l_m} \tag{1}
$$

where F_{max} is the maximum load force (μ N) d_f is the fiber diameter (μ m) \ln is the embedded length of the microdroplet (μ m)

Figure 4. Schematic representation of the single carbon fiber resin microdroplet debonding test. V indicates the direction of the movement of the iron framework (sample holder). Adapted from reference 12 with permission from John Wiley and Sons.

Analogous to IFSS, ILSS is another vital mechanical property of the composites influenced by the sizing agent of the CFs. ILSS of the composites is deduced from the following equation (2) [21]:

$$
ILSS (MPa) = \frac{3P_b}{4dh}
$$
 (2)

where P_b - breaking load at fracture (N) h - width of the specimen (mm) d - thickness of the specimen (mm)

Recent advances in the design of sizing agents for the surface modification of CFs and the corresponding enhancement in the mechanical properties of the CFRPs are summarized in Table 2.

	Sizing compound with structure			Carbon fiber	Performance enhancement of CFRP	Refere nce
Maleic	anhydride	grafted	poly	T300, 3K	42 % enhancement in ILSS	[5]
	(vinylidene fluoride), MPVDF, aqueous					

Table 2. Sizing compounds used for the modification of Carbon fibers.

sizing agent

Sizing plays an important role in improving the interfacial properties of CFRPs. The sizing layer on the CF act as additional compatibilizing phase where in some physical properties (for instance, stiffness modulus) of the composite have gradients, facilitating stress transfer from the polymer matrix to the CFs. In addition, sizing leads to formation of active functional groups on the CF surface enhancing the compatibility of CFs with polymer matrix. Particle size of the sizing agent and its distribution (PSD) is a crucial parameter determining the adhesion, stability, maximum solid content, drying time, rheological and optical properties of the sizing composition. The work of Yuan et al., on the surface modification of CFs with sizing agent (polyacrylate) and engineering the interface of sized CFs and polymer resin matrix (E44, DGEBA) has significantly improved the understanding of the region of interface that is critical for mechanical properties of the CFRPs with applicability in

high technology sectors [24,35]. Sizing emulsions (water borne polyacrylate sizing agent) with five different particle size distributions, PSD, (P1, P2, P3, P4 and P5) with a respective mean particle diameters of 12.32 nm, 95.35 nm, 110.35 nm, 594.28 nm and 1.67 µm were prepared by controlling the PSD by physical filtration through differently sized filter screens (Figure 5). Irrespective of the PSD, all the sizing compositions have a zeta potential (ζ) value of ~ 40 mV with a low value of polydispersity coefficient (0.198-0.217). Usually, ζ value of more than 30 mV imply stability of the emulsion particles due to high electrostatic repulsion. Thus all the sizing emulsions (P1-P5, water borne polyacrylate sizing agents with varying particle size distributions) are thermostable. The aim of the study was to know the effect of PSD of the sizing composition on the adhesion strength of the polymer (epoxy resin) with the CF, and to find the optimal value of the PSD that can fill up the surface defects and interstitial sites on the CF surface and there by enhance the mechanical locking between fiber and the matrix. The authors have judiciously employed various physico-chemical interface characterization techniques like AFM and XPS to study the interface formed by the sizing compound at the interface of the CF and epoxy resin matrix.

Figure 5. Images of the PSD of sizing agents: (a) P-1, (b) P-2, (c) P-3, (d) P-4, (e) P-5; dmean represents the statistical mean diameter of emulsion droplets in different sizing emulsions (water borne polyacrylate sizing agent). Adapted from reference 35 with permission from John Wiley & Sons.

Load and stress transition role of interfacial phase (formed by sizing layer) due to the polarity matching between polymer matrix and sized CF was analyzed by force modulation mode of AFM [35–37]. The stiffness of various phases, namely, the CF reinforcement, the sizing layer (poly acrylate, P5, P3, and P1) on the CF surface and the polymer resin matrix (epoxy E44) as well as the thickness of the interface (formed by the sizing layer that bridges the CFs and the resin matrix) is examined by imaging the phase of the sizing layer at the interface using force modulation microscopy. The change in the stiffness modulus at the interface is a qualitative measure to know the crosslinking density between the fiber and the matrix as well as to understand the transition area between the fiber and the matrix formed by the sizing layer. Using the oscillating cantilever tip that probes the CFRP surface, the stiffness of various phases in the unidirectional CF-epoxy composite is examined. The force modulus images obtained from the cross-section of the composites reinforced by differently sized carbon fibers, namely, with sizing agents P5, P3 and P1 are shown in Figure 6 ac respectively. It should be noted that the relative stiffness image of CF's is brighter than the surrounding epoxy matrix (E44). The corresponding relative stiffness modulus value variation [the gradation of the voltage generated from the cantilever deflection of the AFM as the tip moves from

right (CF phase) to left (epoxy matrix) along the white line (through the interfacial phase of the sizing layer) in the images Figure 6 a-c] at the interface of the sizing layers formed by P5, P3 and P1 (along the white line in the images 6 a-c respectively) is shown in Figure 6. d-f, respectively.

Figure 6. (a, b and c) Relative stiffness image of cross-section areas of P-5, P3 and P-1 sized composites respectively; (d, e and f) stiffness distribution of cross-section in the composites corresponding to (a, b and c respectively; along the white line). Adapted from reference 35 with permission from John Wiley & Sons.

The stiffness image, wherein P5 sizing is employed for the CFs in the CFRP, a clear distinction between the CFs and the surrounding epoxy matrix is observed (Figure 6 a). On the contrary, the boundary between the CF and the epoxy matrix becomes blurrier and a light brown interfacial phase is observed in P3 and P1 sized composites (Figure 6 b and c respectively), signifying the role of optimal particle size distribution (P3 with mean particle diameter of \sim 110 nm) in forming an effective interface between CFs and epoxy matrix. In P5 sized CFRPs (Figure 6d), the magnitude of stiffness modulus drops suddenly (as reflected in the magnitude of current measured in nA and plotted on the Y-axis of Figure 6 d-f), along the white line from right to left. The thickness of the sizing phase at the interface is 0.33 µm which is lower than the thickness of interface formed with sizing agents P3 $(0.39 \,\mu m)$ and P5 $(0.38 \,\mu m)$. These parameters illustrate that large particle size (P5 - 1.67 μ m) of the sizing emulsion plays a negative role in the surface modification (wettability and roughness) and adhesion ability of CF surface with the epoxy resin matrix. In contrast, the stiffness modulus at the interface of CFRPs sized with P3 and P1 sizing agents decrease gradually (from right to left, from CF surface to the matrix along the white line in the images Figure 6 e-f respectively) indicating the gradient sizing distribution in the interface layer forming thicker interface ($\sim 0.39 \,\mu m$). Thus relatively small size (~ 110 nm, P3) sizing droplets particles of the polyacrylate spread out on the CF surface uniformly healing the penetrating into the surface defects and interstitial sites facilitating the stress transfer efficiency. These observations were further confirmed by the evaluation of IFSS values of CFRPs without sizing agent (81.2 MPa) and CFRPs sized with P1-P5 sizing compounds (88.3-92.5 MPa). The CFRPs sized with P3 showed a 13.9 % enhancement compared to unsized CFRPs (with no sizing agent) and 4.7 % enhancement compared to P5 sized CFRP's [10].

The geometry and location of sizing agent/compound and the mechanism of interlocking of CF and resin matrix through sizing agent (poly acrylate) at the interface with optimal PSD was demonstrated by Yuan et al., in the typical example of CF-epoxy (E44) composite [35].

Sizing agent with optimal multimodal PSD fit into the defects and interstices on CF surface and increase the packing efficiency and uniformity of surface distribution. The surface groves and defects of CFs are reduced and rectified. Relatively small particle size of sizing agent (~110 nm as in the above example) results in the formation of interface of moderate thickness and even distribution of sizing compound permeating through the bundles of CFs. As a result, surface defects are reduced, chemically active surface is formed leading to strong interfacial adhesion and effective stress

transfer from polymer matrix to CF and thereby the load bearing ability with high tensile strength of CFs is utilized in various applications as metal replacement [35]. The chemical interlocking (by covalent and hydrogen bonding interactions) of the CF surface and epoxy matrix is facilitated by the increase in oxygen functional groups at the interface due to sizing by polyacrylate emulsion particles of optimum PSD (~ 110 nm) as deduced from XPS analysis [35].

2.2. Physical and Chemical Methods of Surface Modification of Carbon Fibers:

Apart from sizing, a variety of chemical and electrochemical methods were recently developed for the surface modification of carbon fibers. Vedrtnam and Sharma classified surface modification methods into five broad classes, namely, wet methods (sizing, electrochemical, acid treatment), dry methods (plasma, thermal, high energy irradiation), using nanomaterials (CNT's , ZnO, TiO2, SiO2, SiC, graphene oxide), oxidative methods (oxidation with acids, gases, plasma) and nonoxidative methods (pyrolytic carbon deposition, plasma polymerization, whiskerization) [38]. Zang et al., reviewed the progress in carbon fiber surface modification methods, namely, grafting, coating, oxidation, and plasma treatment and proposed that chemical grafting method standout owing to its advantages (precision of grafting polymeric species on to CF surface) resulting in improvement in surface roughness, and mechanical properties (interfacial adhesion) in composites [39]. Zang et al., classified surface modification methods into three groups, namely, wet modification methods (liquid phase oxidation, anodic electrolytic oxidation and sizing treatment), dry modification methods (gas phase oxidation, plasma oxidation and irradiation treatment) and nanoparticle modification (functionalization with graphene, CNT and metal oxide NPs). Merits and demerits of various modification methods for application of modified CF's for carbon fiber reinforced polyamide (CFRPA) were discussed [40]. Raphael et al., pointed out that grafting is an effective and efficient alternative to oxidation functionalization for the surface modification of CF [41]. Raphael et al., reviewed various methods of modification of CF and the resulting property enhancement for the reduction of interfacial tension so as to utilize the potential of the reinforcing matrix to the fullest. The authors have classified surface modification methods into five groups, namely, electrochemical oxidation, chemical oxidation, plasma treatment, gamma ray or laser irradiation and treatment with rate earth elements [41]. Hung et al., reviewed method of surface modification of CF's with graphene-related materials (GRM) derived from graphite. GRM are effective in improving the properties of the CF's in stress transfer from matrix to the CF through the interface comprising of GRM. The authors pointed out that the property enhancement of the composite materials under cryogenic environment are crucial for new applications involving aircraft and space engineering development [42]. Corujerira-Gallo reviewed the changes in the surface chemistry and surface microstructure of CFs as a result of plasma treatment. Surface contaminants or weekly bonded graphitic layers are removed by the process of etching, surface roughness increased, the surface chemistry and the polarity are altered [43]. Naito reviewed the effect of surface modification of CFs, by grafting with CNTs, coating with polymeric materials and other hybrid methods, on the resulting tensile properties of both pitch and PAN based CF's. A linear relationship between Weibull modulus and average tensile strength on a log-log scale was observed for all surface modified CFs. While all modifications resulted in improvement of tensile strength and Weibull moduli, hybrid modifications (grafting followed by vapour deposition, grafting-dipping hybridization) resulted in the highest values [44]. An exemplary account of the chemical and electrochemical methods invented for the surface modification of carbon fibers enhencing their applicability is provided in Table 3 and Table 4 respectively.

Table 3. Chemical methods for the surface modification of carbon fibers.

Carbon fibers	Chemical method	Functionality improvement	Reference
		CFs were obtained Salicylaldehyde (SLDH) was Contact angle with water decreased from [45]	
		from Toray industries grafted chemically through 3- 78.5 to 52.1° and the surface energy	
(diameter, 7 $µm$;		aminopropyltriethoxyilane $(3-$ increased from 35.9 to 55.0 mNm ⁻¹ ; IFSS of	
		tensile strength, 3500 APS) bridges onto the surface of the composite (CF-g-SLDH and methyl	
MPa)	CFs	phenyl silicone resin, MPSR) was enhanced	

2.3. Surface Modification of Carbon Fibers with Nanoparticles:

Kakhki reviewed the surface modification of CFs by enzymes and nanoparticles (like Pt, Rh, Au) for enhanced performance of the modified CF's as electrodes with application in analytical chemistry, electrochemistry, environmental chemistry, health science, and renewable energy (battery, supercapacitors, fuel cells and biofuel cells) [155]. Vedrtnam and Sharma reviewed the potential of nanospecies (CNTs, ZnO nanorods, SiO2 nanotubes) in the surface modification of CFs for enhancing the performance (interfacial strength, vibration attenuation and delamination resistance) of the resulting CFRPs and proposed that the potential of CNTs is underutilized for modifying CF surface [38]. A brief account of the recent advances in the surface modification of carbon fibers with nanoparticles is provided in Table 5.

Carbon fibers	Modification method	Functionality enhancement	Referenc
			e
Carbon fibers from Donghua university (no further details available)	Hydrophilic Fe3O ₄ NPs were grafted on the surface of CFs polyol-assisted using hydrothermal method (CFs@ $Fe3O4$;	Presence of hydrophilic Fe3O4 NPs improved interfacial adhesion of CFs; Hydrophobic CFs were converted to hydrophilic magnetic CF, CFs@Fe3O4@SiO-C/Ni;	$[156]$
T300, diameter 7 µm, provided by Toray, Tokyo, Japan	Coating nanoparticles of polyetherimide (PEI) on carbon fibers by evaporation induced surface modification;	IFSS enhanced by 20.5, 37.7, 52.7, 49.6, 42.5 and 58.0 % as the thermoplastic resin in the composite is varied from PVC, PC, PA6, PP, PA66 to PEI respectively	$[157]$
Carbon fibers further (no details provided)	Desized carbon fibers added to a solution (solvent is atleast one of water, alcohol, acetone, and tetrahydrofuran) of ferrocene derivative Subsequently the ferrocene functionalized CFs either oxidized were or electrooxidized	Though not disclosed, the surface modification of CFs might have formed nanoparticles of FesO ₄ on CF surface making the CFs magnetic and hydrophilic leading to enhancement of their performance in composite materials and catalysis.	[158]
T300 (average filament 7 diameter $µm$); 3 K plain mat weave carbon type tensile fibers; strength, ~3500 MPa; supplied Toray, by Japan	Grafting graphene based nanofillers to CF surface by cathodic electrophoretic deposition (EPD)	IFSS and flexural strength of composite (CF-DGABE type epoxy) enhanced by 35 and 26.6 % respectively	$[159]$

Table 5. Nanoparticles functionalized carbon fibers.

2.4. Discussion and Summary:

Surface modified carbon fibers (SMCFs) influence almost all spheres of human life by improving the standing of living and alleviating the suffering of mankind. Advent of materials based on SMCFs is envisioned to revolutionize the chemical, energy, environment, health, infrastructure, materials, agricultural, defense and chemical industries in new and incomprehensible ways owing to drastic enhancement in the properties and the resulting multi functionality of these materials. Representative examples of the application of SMCFs revolutionizing various industries are as shown in Schemes 1- 5 and are self-explanatory.

Scheme 1. Revolutionary applications of surface modified Carbon fibers (SMCFs) in health

Scheme 3. Revolutionary applications of surface modified Carbon fibers (SMCFs) in environment

Scheme 4. Revolutionary applications of surface modified Carbon fibers (SMCFs) in defense

Scheme 5. Revolutionary applications of surface modified Carbon fibers (SMCFs) in catalysis

Scheme 6. Revolutionary applications of surface modified Carbon fibers (SMCFs) in smart materials

Common organic precursors used for the production of CFs include polyacrylonitrile (PAN) and pitch with a market share of 97 and 3 % respectively. Owing to their low price and wide availability PAN based CFs (20 ϵ /kg) CFs are extensively studied and used compared to pitch based fibers (100 ϵ /kg) as evident from the research findings summarized in Tables 3 & 4. However, diverse methods are being developed to produce CFs with varying properties [200]. Effect of surface modification method is substrate (CF) specific and cannot be generalized. This is evident from the specific example of physical activation methods (NH3 plasma, O2 plasma, air plasma, electrolysis) employed with carbon fibers of equivalent (electrode surface and material) properties, namely, HTS40 and CT50. Significant effects of activation were observed in the case of CT50 while the effects of activation were only marginal in HTS40. Compared to CT50, HTS40 showed better electrode performance when used as electrode material for bio electro chemical systems (BES). Carbon fiber properties influenced the bacterial (Shewanella Oneidensis MR-1) current generation properties. Potschke et al., reviewed the selection criteria of CFs for application as electrode material, especially for BES. Commercial CFs namely, HTS40, CT50 and T300 were supplied by Teijin carbon Europe Gmbtt, Japan/Germany, SGL carbon, Germany, and Toray Industries Inc., Japan were studied. Effect of physical activation and desizing on electrode performance were examined. Surface activation was found to reduce the startup time while its impact on maximum current density could not be ascertained [200]. On the contrary, removal of sizing (protective coating) of CFs is very vital

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for all the fibers studied for BES application and such desizing enhanced he maximum current density up to 40 fold. Exact composition of the sizing is a subject of intellectual property rights (IPR) of the industries. In the specific example of T300 fabrics, highest desizing (83.3 %) is achieved by pyrolysis in inert atmosphere (N_2 , 500 °C, 20 min) resulting in 45 fold enhancement in BES performance. A combination of free filament ends and high degree of graphitization enhanced the electrode performance by 100 %. This is to demonstrate that the selection of CF (substrate) influences the electrode performance.

The method of surface modification of CFs is application specific. No single modification methods is applicable for generating the desired functionality on CFs that suits all the demanding applications. As a result there is scope for further development of surface modification methods as diverse as the target applications, demands, challenges and needs of human societies. However, generalizations can be drawn for the knowledge generated by research and development in the field, especially over the past decade (2010-2010). Even though, a web of Science search with the keywords, namely, "carbon fibers" and surface modification", yields 3044 results, these results could be further screened out to few hundred papers based on major advances made in this field. The summon substance of such screened out results, is that the applicability of CFs can be drastically enhanced in astonishing ways by surface modification. Essentially, surface modification methods impart polarity (oxygen functionality; presence of metal NPs; grating of carbon nanomaterials; coating of functional polymers) to the CF surface which is otherwise inert and non-reactive.

Commercial significance of the surface modification of CFs is evident from the very many patents issued on this subject recently [201–278]. A glimpse of the kind of surface modifications reported in patent literature are highlighted in Table 6.

Table 6. Highlights of the surface modification methods developed in patent literature (2020-2010).

Desizing, oxidation (conc HNO₃ treatment), amination (by treatment with 3- [246] amino propyl triethoxy silane) grafting graphene oxide; wettability and surface roughness enhanced; strength enhanced by 20-50 %; toughness enhanced by 35- 40 %

Grafting of methyl methacrylate (MMA) monomer to Ni (submicron) coated CF; [248] application in high temperature plastics with electromagnetic shielding potential

Anode electro oxidation in the presence of ammonium bicarbonate; graphite plate [250] used as cathode in the anodized surface treatment

Hydroxy functionalized CF (by treatment with ethanol) and grafting acrylate [252] monomer followed by oxidation with inert gas plasma; modified CFpolycarbonate composite find application in electric, aerospace, military and chemical industries

Desizing, oxidation, acylation and grafting bis (3-aminophenyl) phenyl [253] phosphine oxide

anhydride/acrylic acid) by atomizing spray nozzle, wettability, surface energy

CNT's were grown on CF surfaces by chemical vapour deposition with Ni catalyst [278]

Research and development, especially on the surface modification of carbon fibers, is intensifying as evident from the increasing trend in the publications in this field with time. A web of Science search with the keywords, "carbon fibers" and "surface modification" for the years from 2010 to 2021 shows growing interest in field of "Carbon fiber surface modification" as shown in Figure 7.

Figure 7. Growing interest in the research field of "Surface modification of carbon fibers" during 2010-2021.

For further knowledge on the surface modification of carbon fibers by physical (plasma, microwave, electron and gamma ray, laser irradiation), chemical (sizing, oxidation with mineral acids, nanoparticle deposition, grafting of polymers, amine and oxygen functionalization), electrochemical (oxidation, in situ polymerization, grafting) methods, leading to the generation of surface polarity, improving surface roughness, energy and wettability and inducing multifunctionality, and enhancing the mechanical properties of the CF reinforced composites by improving the interfacial adhesion, the readers are directed to the following literature published during 2015-2010 [279–365]. Moreover, a bibliography of the latest updates in the field of surface modification of carbon fibers during the past two years (2021-2022) has also been provided [365–459].

Conclusion:

Literature on the subject of "surface modification of carbon fibers" over the past decade (2020- 2010) is critically reviewed. Grafting was pointed out be some reviewers on this subject as the ideal surface modification method for CFs. However, recent evolution in this field, during the past decade, clearly demonstrate that hybrid surface modification methods are the future, meaning, a combination of two or more methods like oxidation, followed by grafting; grafting followed by coating; oxidation followed by electro polymerization should be adopted. Moreover, the method of modification is application specific. Depending on the problem at hand and the need, the functionality (modification method) need to be tuned. The 459 research findings reviewed in this paper provide the needed guidance to researchers and industrial practitioners working with carbon fiber based materials, for fine tuning of surface modification methods depending on the application. The method of surface modification of CFs is application specific. No single modification method is applicable for generating the desired functionality on CFs that suits all the demanding applications. As a result there is scope for further development of surface modification methods as diverse as the target applications, demands, challenges and needs of human societies. However, generalizations can be drawn for the knowledge generated by research and development in the field, especially over the

past decade (2010-2020). Even though, a web of Science search with the keywords, namely, "carbon fibers" and surface modification", yields 3044 results, these results could be further screened out to few hundred papers based on major advances made in this field. The summon substance of such screened out results, is that the applicability of CFs can be drastically enhanced in astonishing ways by surface modification. Essentially, surface modification methods impart polarity (oxygen functionality; presence of metal NPs; grating of carbon nanomaterials; coating of functional polymers) to the CF surface which is otherwise inert and non-reactive.

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